

### •••• Forgot to mention yesterday.....

- HIRLAM scientific documentation (2002):
- Go to <u>www.hirlam.org</u>
- Documentation
- Scientific documentation (large pdf-file)



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- And then for those of you who can stay awake:

#### Contents of lecture



- Importance of vertical diffusion scheme
- Vertical diffusion, flux calculations
- 1<sup>st</sup>, 2<sup>nd</sup> and 3<sup>rd</sup> order schemes
- Local and non-local schemes
- HIRLAM CBR
- Dry and wet conservative parameters
- Characteristics of HIRLAM vertical diffusion

# •••• Importance of vertical diffusion

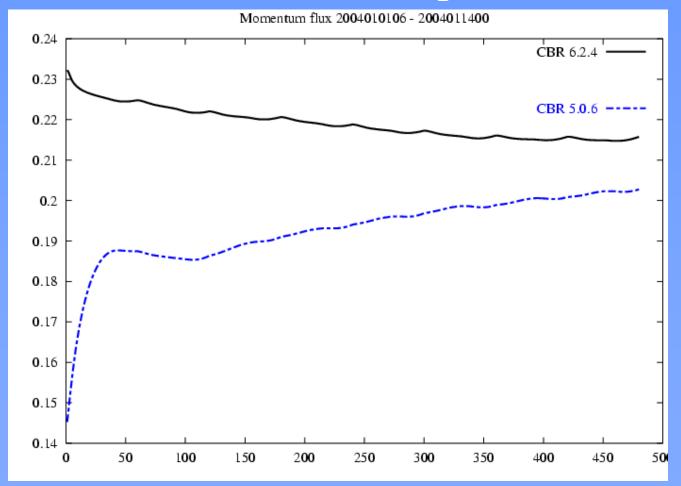


- Vertical diffusion scheme determines the characteristics of the boundary layer in NWP-models
- Also impact on synoptic scale behaviour of model
- Too weak mixing: too little Ekman pumping and low pressure systems becoming too intense, increasing activity in model during forecast, chance of decoupling of surface and atmosphere
- Too much mixing: too deep boundary layer, especially for stable (very sensitive) conditions, can have large impact on ACT modelling
- Most NWP-models have too much mixing in stable conditions

# •••• Impact of vertical diffusion



#### • From too active to too damped





- Vertical transport due to turbulence, example potential temperature:
- First law of thermodynamics:

$$\frac{\partial \theta}{\partial t} + U_j \frac{\partial \theta}{\partial x_j} = \frac{1}{\rho C_p} \left[ L_v E + \frac{\partial Q_j^*}{\partial x_j} \right]$$

• Continuity equation:

$$\frac{\partial \rho}{\partial t} + U_j \frac{\partial \rho}{\partial x_j} = -\rho \frac{\partial U_j}{\partial x_j}$$

• Reynolds decomposition

 $\theta = \overline{\theta} + \theta', \quad \overline{\theta'} = 0$ 

• First law of thermodynamics

$$\frac{\partial \overline{\theta}}{\partial t} + \overline{U}_j \frac{\partial \overline{\theta}}{\partial x_j} + U'_j \frac{\partial \theta'}{\partial x_j} = \frac{1}{\rho C_p} \left[ L_v E + \frac{\partial Q_j^*}{\partial x_j} \right]$$

• Incompressible continuity equation:

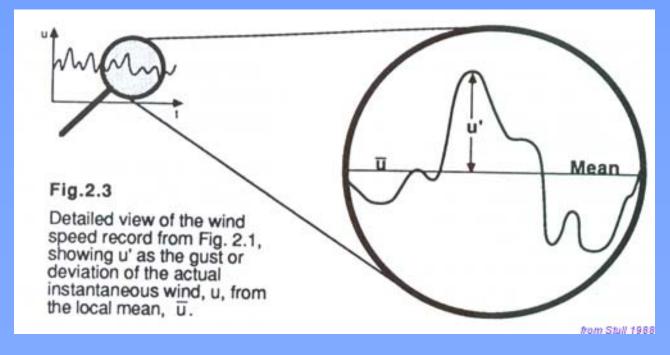
$$\frac{\partial(\overline{u}+u')}{\partial x} + \frac{\partial(\overline{v}+v')}{\partial y} + \frac{\partial(\overline{w}+w')}{\partial z} = 0$$

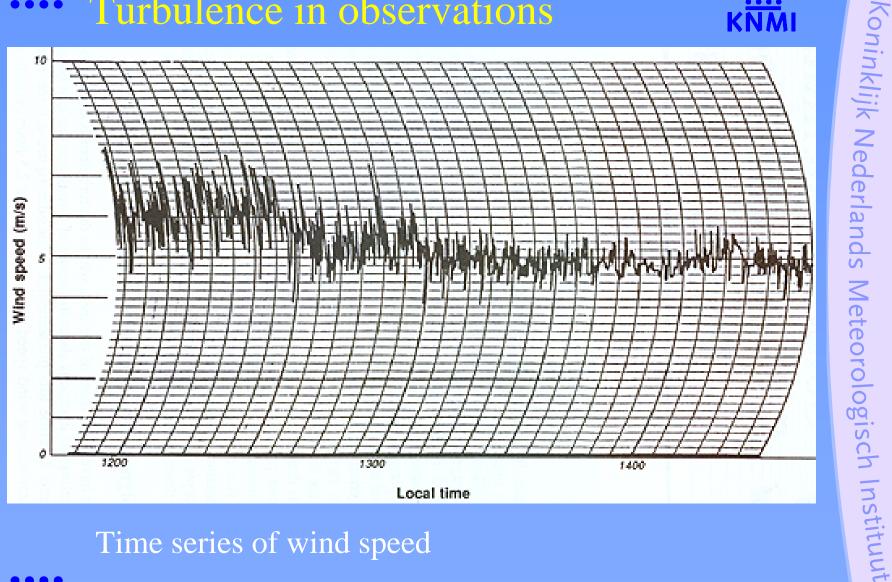




• Splitting into average and turbulent part (Reynolds decomposition)

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = 0 \quad and \quad \frac{\partial u'}{\partial x} + \frac{\partial v'}{\partial y} + \frac{\partial w'}{\partial z} = 0$$





#### Turbulence in observations $\bullet \bullet \bullet$

• First law of thermodynamics

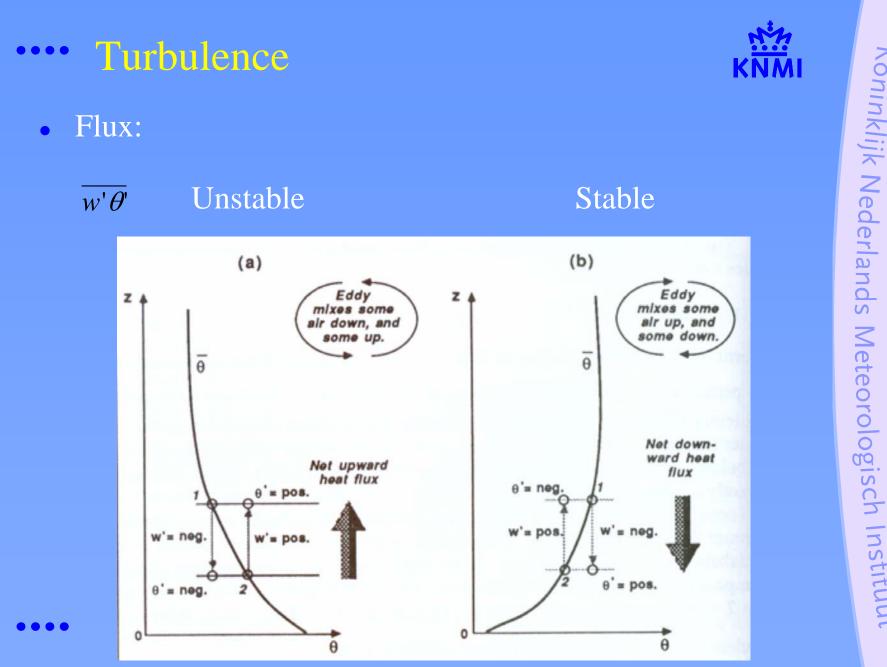
$$\frac{\partial \overline{\theta}}{\partial t} + \overline{U}_j \frac{\partial \overline{\theta}}{\partial x_j} + \left( \frac{\partial \overline{U}_j \overline{\theta}}{\partial x_j} \right) = \frac{1}{\rho C_p} \left[ L_v E + \frac{\partial Q_j^*}{\partial x_j} \right]$$

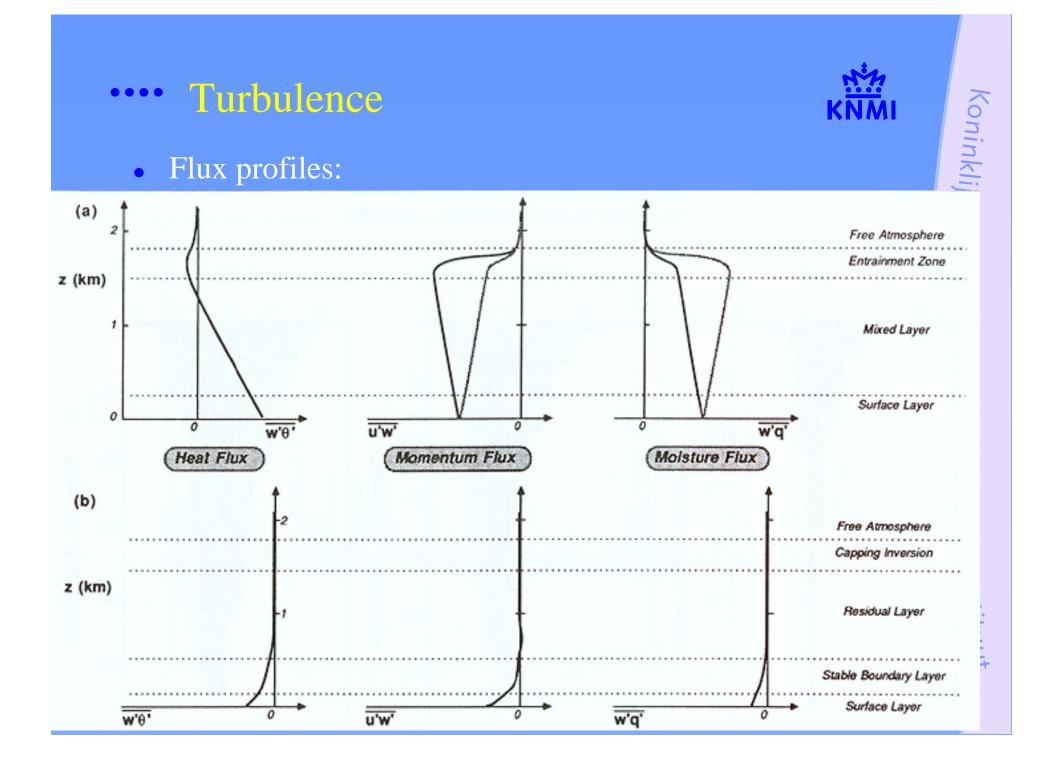
• Turbulent flux term in vertical direction:

$$\frac{\partial \theta}{\partial t} = -\frac{\partial \overline{w' \theta'}}{\partial z}$$

• In synoptic scale NWP-models horizontal turbulent terms are usually ignored









- How to calculate the flux from the model profile, that represents average conditions -> vertical diffusion scheme.
- Options: 1<sup>st</sup> order, 2<sup>nd</sup> order or 3<sup>rd</sup> order. Order dependent on where closure for new parameter (flux) is put.
- First order: flux calculated directly from profiles of wind and temperature
- Second order: flux dependent on another extra parameter: Turbulent Kinetic Energy (TKE). Closure in description of parameters determining TKE



• Higher (third) order: TKE dependent on production and destruction terms. Production and destruction are calculated explicitly. Closure in parameters determining production and destruction. Other correlation terms are taken into account



• First order scheme (local):

$$w'\theta' = -K_h \frac{\partial \overline{\theta}}{\partial z}$$

• Combination of eddy diffusion coefficient and gradient in average potential temperature

 $K_h = l_h^2 SF_h(Ri)$  Louis et al, 1982

- $l_h$ : length scale; S: shear;  $F_h$  function dependent on Richardson number
- First scheme in HIRLAM

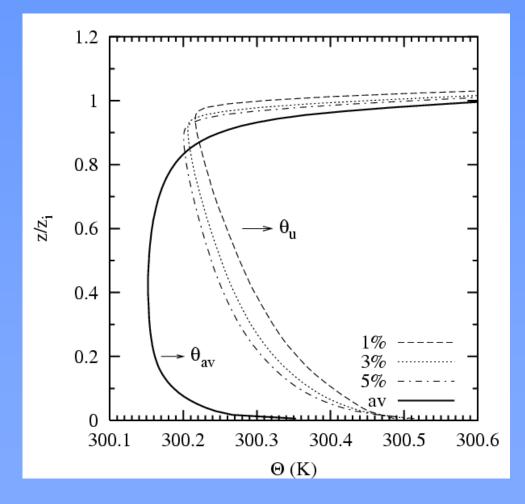


• First order scheme (non-local, K-profile):

$$w'\theta' = -K_h \frac{\partial \overline{\theta}}{\partial z} + \overline{w'\theta'}_{NL}$$

- Similar to local scheme, with addition of non-local flux term to take counter gradient flux into account  $K_{h} = kw_{t}z\left(1 \frac{z}{h}\right)^{2}$ Troen and Mahrt, 1986
- z: height, *h*: boundary layer height, *w<sub>t</sub>*: turbulent velocity velocity scale

### Non-local flux



Potential temperature profiles in boundary layer eddies, average and in strongest ..% of updrafts (from LES)



• Non-local flux part:

 $\overline{w'\theta'}_{NL} = K_h a \frac{w_* (\overline{w'\theta'})_0}{w_m^2 h} \quad \text{Holtslag and Boville, 1993}$ 

- Non-local part gives fluxes that are caused by the strongest eddies in boundary layer.
- Non-local scheme works due to smart choice of profile of K<sub>h</sub> strongly dependent on boundary layer height!
- Second scheme in HIRLAM

#### •••• TKE-schemes



- TKE: Turbulent kinetic energy, measure for amount of turbulence (and mixing) in atmosphere
  - Strong correlation with transport in atmosphere
  - TKE-tendency important. TKE decreasing-> boundary layer becoming less turbulent. TKE increasing-> boundary layer bcoming more turbulent.
  - Different processes that produce and destroy TKE
- Definition TKE:

$$\frac{TKE}{m} = \frac{1}{e} = 0.5(u'^2 + v'^2 + w'^2)$$

#### ••••• TKE (2)



$$\frac{\partial \overline{e}}{\partial t} = -\overline{u}\frac{\partial \overline{e}}{\partial x} + \frac{g}{\theta_{v}}(w'\theta') - \overline{u'w'}\frac{\partial \overline{u}}{\partial z} - \frac{\partial \overline{w'e'}}{\partial z} - \frac{1}{\overline{\rho}}\frac{\partial(w'p')}{\partial z} - \varepsilon$$

$$1 \quad 2 \quad 3 \quad 4 \quad 5 \quad 6 \quad 7$$

- 1: local change of TKE
- 2: advection of TKE
- 3: buoyancy production/destruction
- 4: shear production
- 5: vertical diffusion of TKE

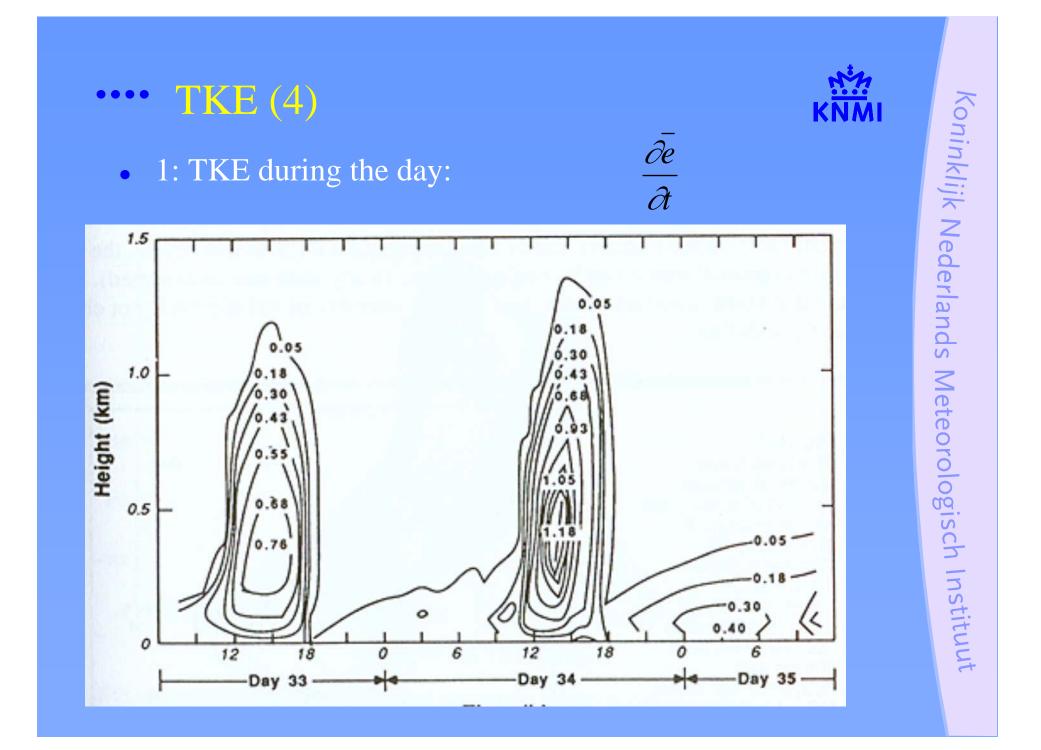
#### •••• TKE (3)



$$\frac{\partial \overline{e}}{\partial t} = -\overline{u}\frac{\partial \overline{e}}{\partial x} + \frac{g}{\theta_{v}}(w'\theta') - \overline{u'w'}\frac{\partial \overline{u}}{\partial z} - \frac{\partial \overline{w'e'}}{\partial z} - \frac{1}{\overline{\rho}}\frac{\partial(w'p')}{\partial z} - \varepsilon$$

$$1 \quad 2 \quad 3 \quad 4 \quad 5 \quad 6 \quad 7$$

- 6: pressure-correlation
- 7: dissipation
- Equation describes all sources and sinks of TKE:





- CBR: Cuxart, Bougeault and Redelsperger (2000)
- In TKE scheme flux is calculated through:

$$w'\theta' = -K\frac{\partial\theta}{\partial z}$$

• The eddy diffusion coefficient is given by:

 $K = l\sqrt{\overline{e}}$ 

- The diffusion therefore is a function of the TKE, a length scale and the gradient of the parameter that is diffused
- Mixing very sensitive to TKE and 1 in stable conditions



• Length scale in eddy diffusion coefficient:

$$\frac{1}{l_{m,h}} = \frac{1}{\max(l_{\text{int}}, l_{\min})} + \frac{1}{l_s}$$

• Minimum length scale:

$$\frac{1}{l_{\min}} = \frac{1}{l_{\lim}} + \frac{1}{c_n \kappa z}$$

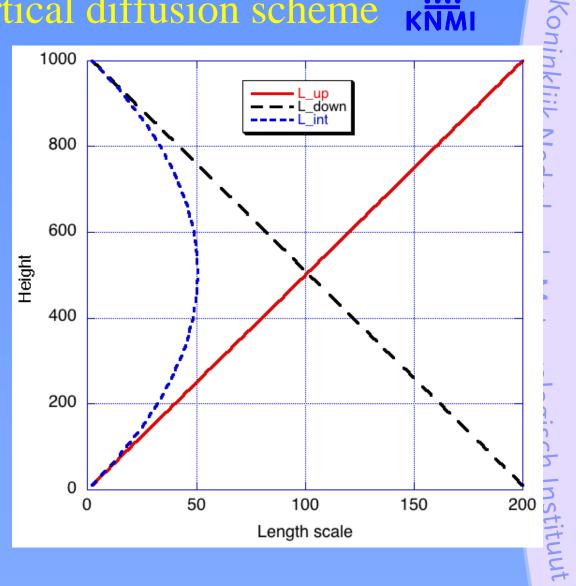
• Stable length scale:

$$\frac{1}{l_s} = c_{m,h} \frac{\sqrt{e}}{N}$$



• Integral length scale

 $\frac{1}{l_{int}} = \frac{1}{l_{up}} + \frac{1}{l_{down}}$ with  $l_{up}(z)$  integral from surface to z of stability F(N), similar for  $l_{down}$ 

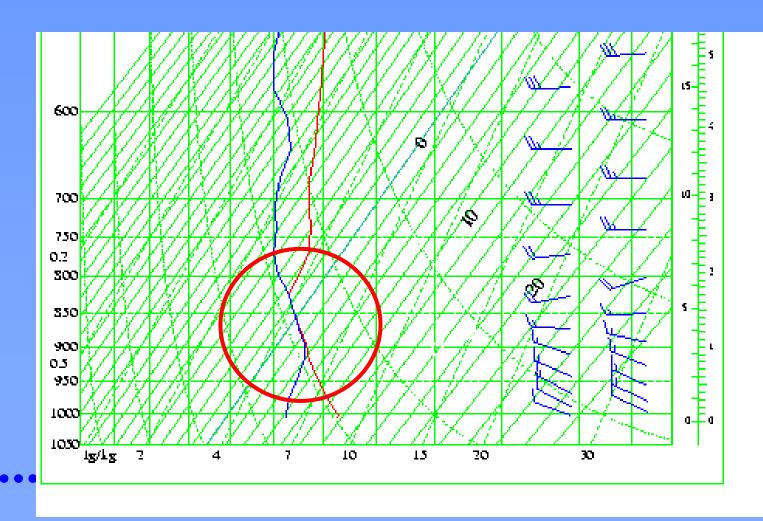


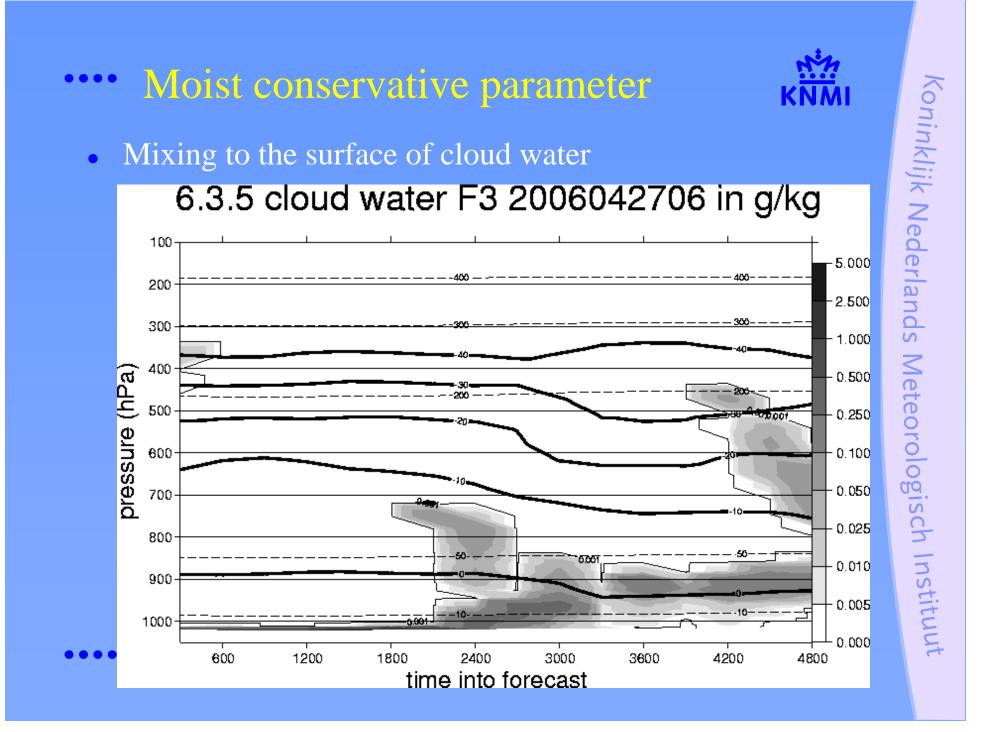
# •••• Moist conservative parameter

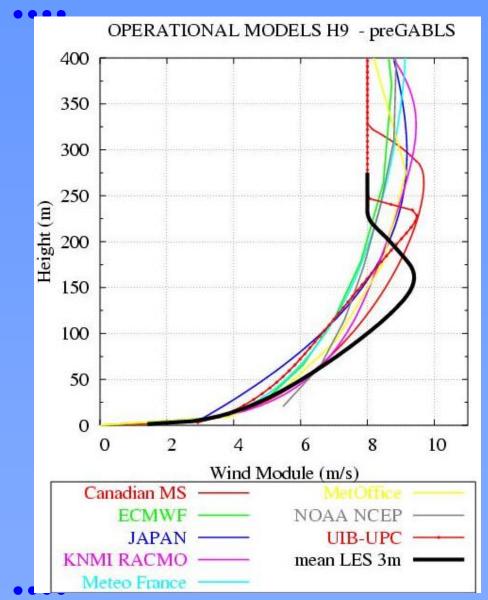


- Until HIRLAM 7.2 stability in vertical diffusion scheme dependent on dry potential temperature
- Can lead to dry adiabatic profile in saturated environment (stratiform clouds) with cooling at cloud top
- Convection parameterization taking over where there should only be large scale clouds
- Use of liquid potential temperature leads to more mixing in moist conditions such as stratus, stratocumulus and fog

- •••• Moist conservative parameter
  - Dry unstable profile in moist conditions







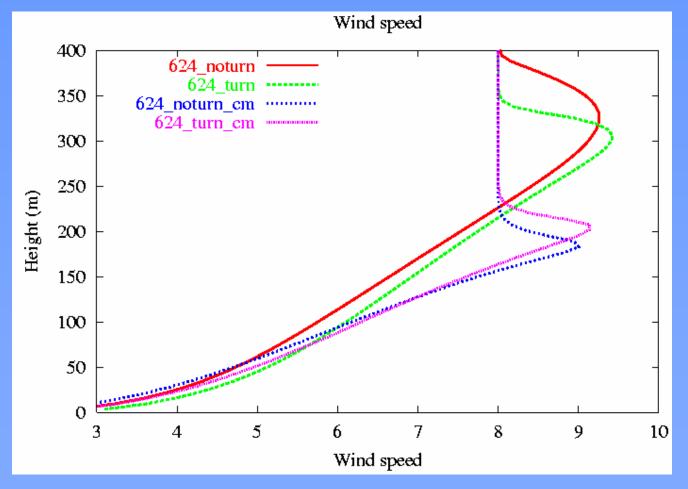
Intercomparison (GABLS 1) shows weaknesses of models: too much mixing in stable conditions

## •••• Conclusions GABLSI

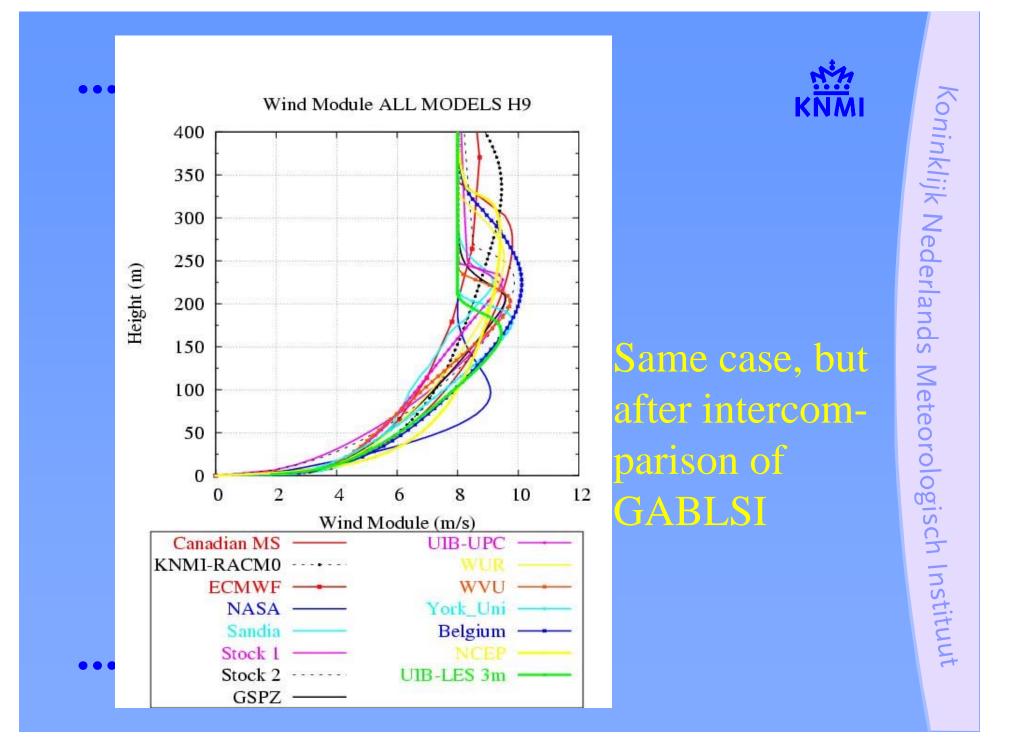


- None of the operational models was able to describe wind profile properly
- Stable boundary layer too thick
- Cooling over too thick layer, too much energy taken out from the atmosphere
- Windmaximum at too high level in atmosphere (steady state experiment, impact on max wind speed small)
- Increase in wind and temperature close to the surface too small, wind near surface too strong

HIRLAM before and after GABLSI KNN extra tuning necessary for good synoptic behaviour

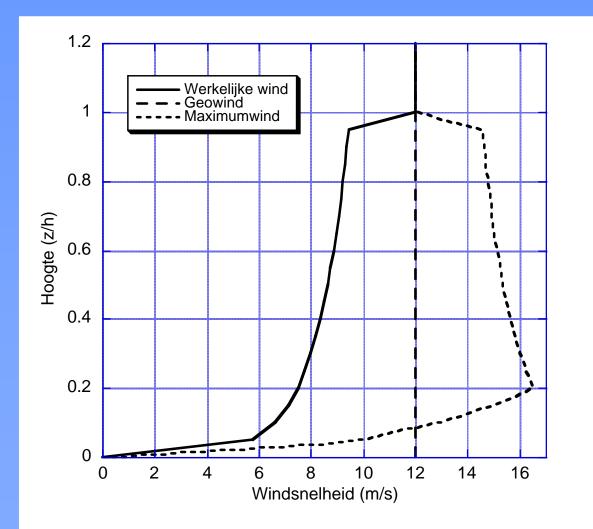


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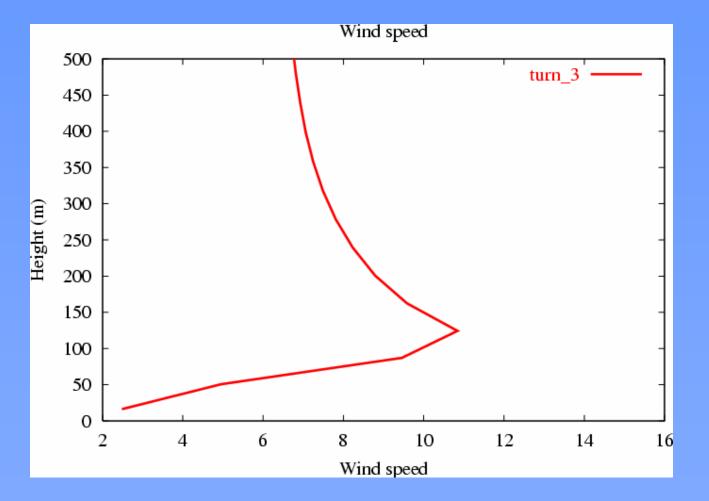
KNMI

#### •••• Low level jet

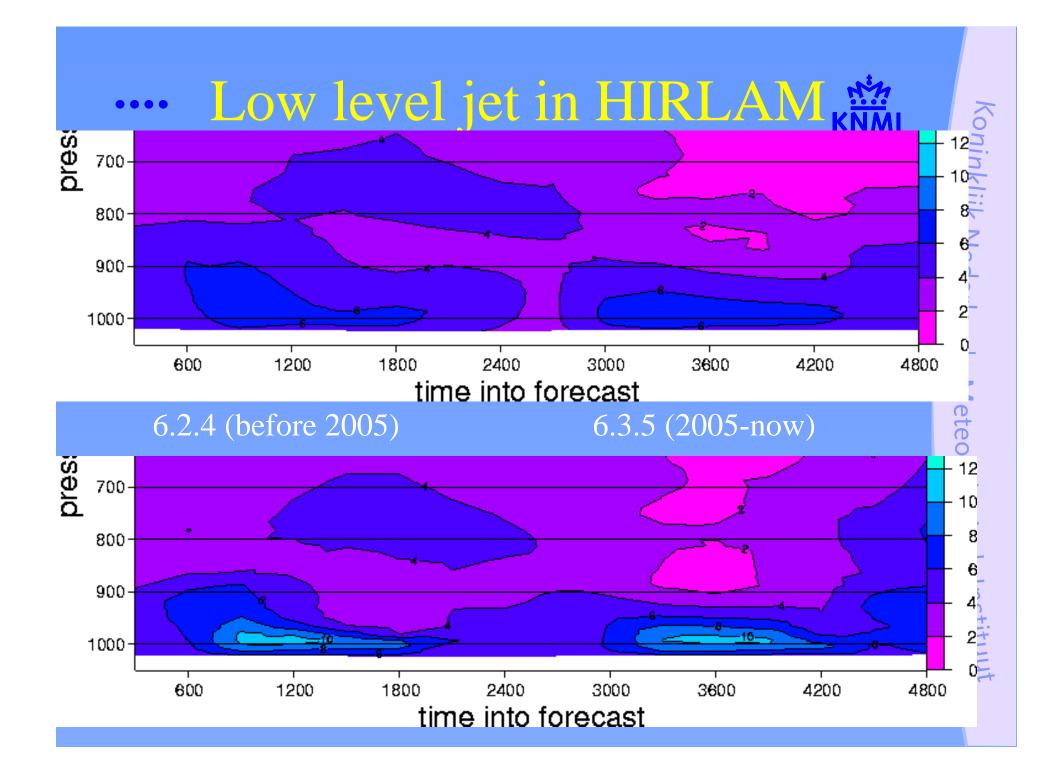


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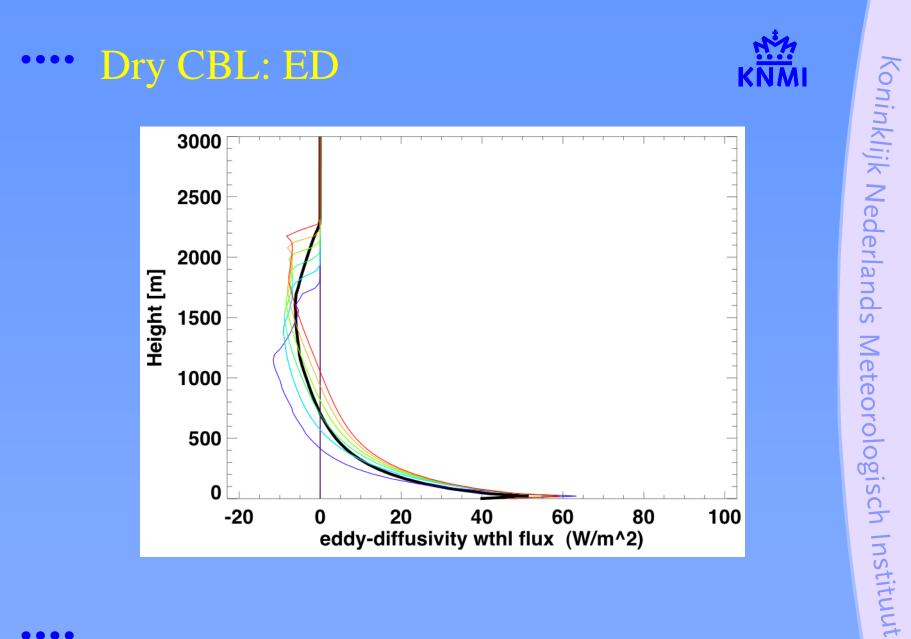
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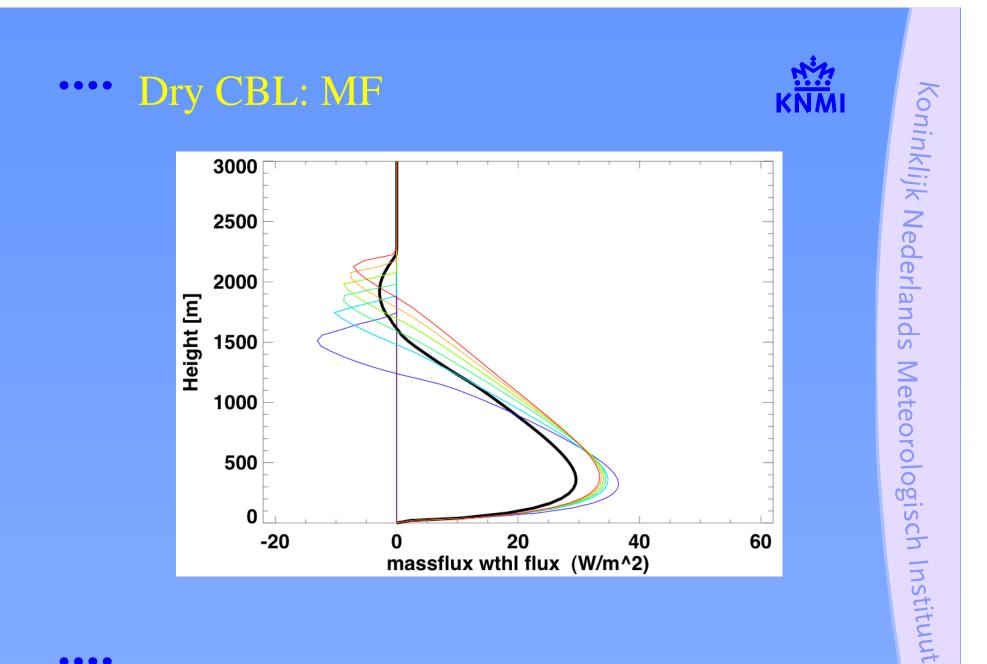
# •••• New development: EDMF

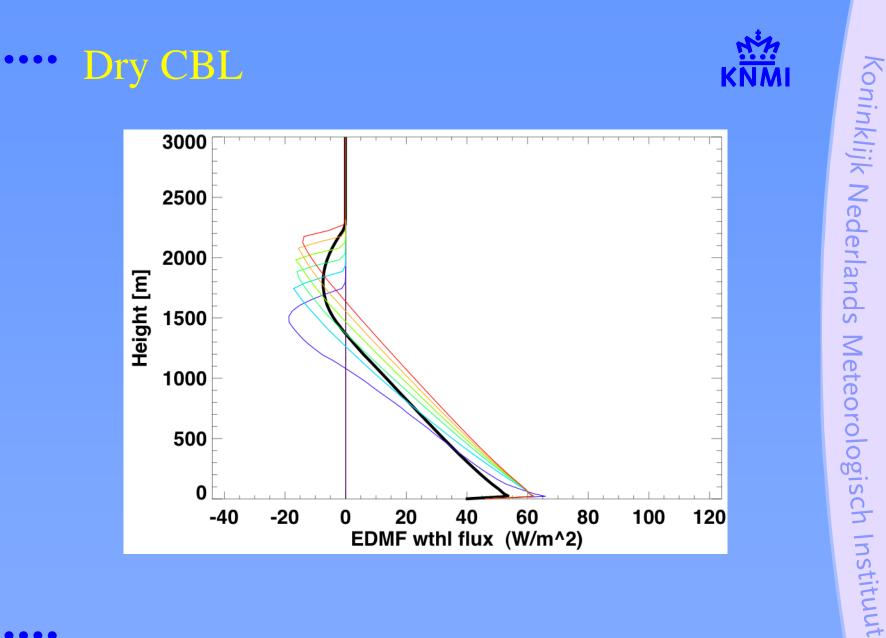
KNMI

- Eddy diffusion mass flux scheme
- Mass flux describes transport due to strongest eddies
- Eddy diffusion scheme describes local transport caused by smaller eddies
- Mass flux scheme can also handle shallow moist convection, cumulus clouds etc. No additional scheme necessary for shallow convection, natural connection between boundary layer and shallow convection
- Mass flux scheme describes non-local transport, relatively large transport with slightly stable profile.
- PBL-scheme for HARMONIE, maybe also for HIRLAM.



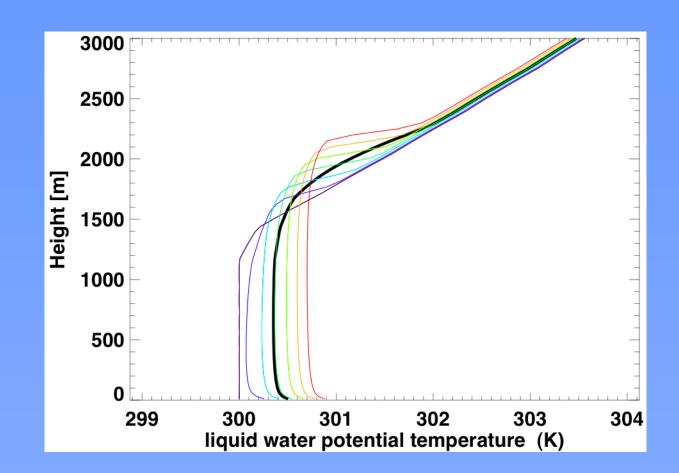
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•••• Dry CBL: T-prof





• CBR: Cuxart, Bougeault and Redelsperger (2000)

$$-\left[u'w'\frac{\partial u}{\partial z} + v'w'\frac{\partial v}{\partial z}\right] = K_m \left[\frac{\partial^2 u}{\partial z^2} + \frac{\partial^2 v}{\partial z^2}\right]$$

$$\frac{g}{\theta_{v}}\overline{w'\theta_{v}'} = -K_{h}\frac{g}{\theta_{v}}\frac{\partial\theta_{v}}{\partial z}$$

$$-\frac{\partial \overline{w'e'}}{\partial z} - \frac{1}{\overline{\rho}} \frac{\partial \left(\overline{w'p'}\right)}{\partial z} = 2K_m \frac{\partial \overline{e}}{\partial z}$$

$$\varepsilon = c_d \frac{\left(e\right)^{3/2}}{l_m}$$